

# Full-scale Mars Science Laboratory Tiled Heatshield Material Response

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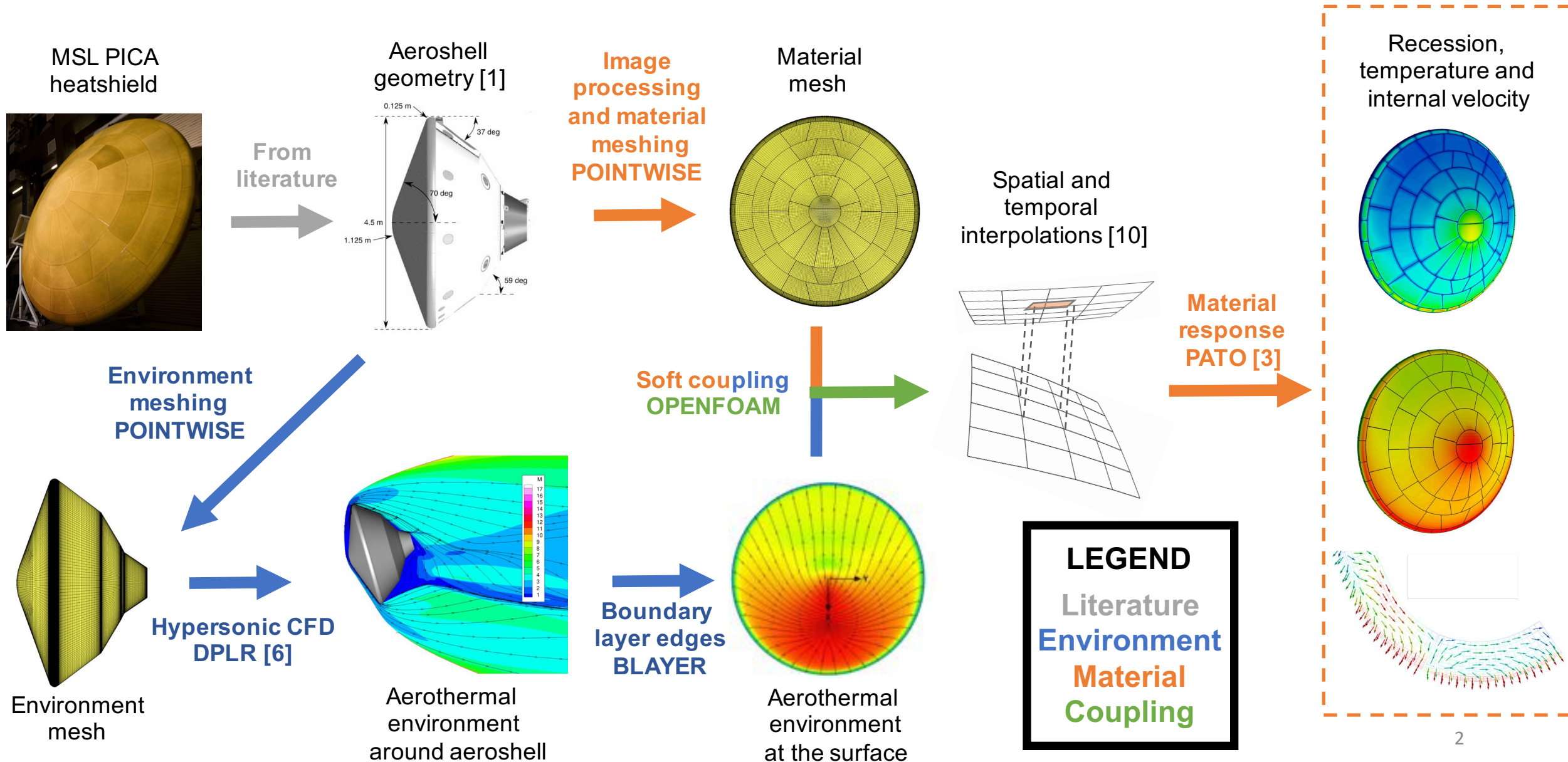
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# Overview – Coupling aerothermal environment and material response

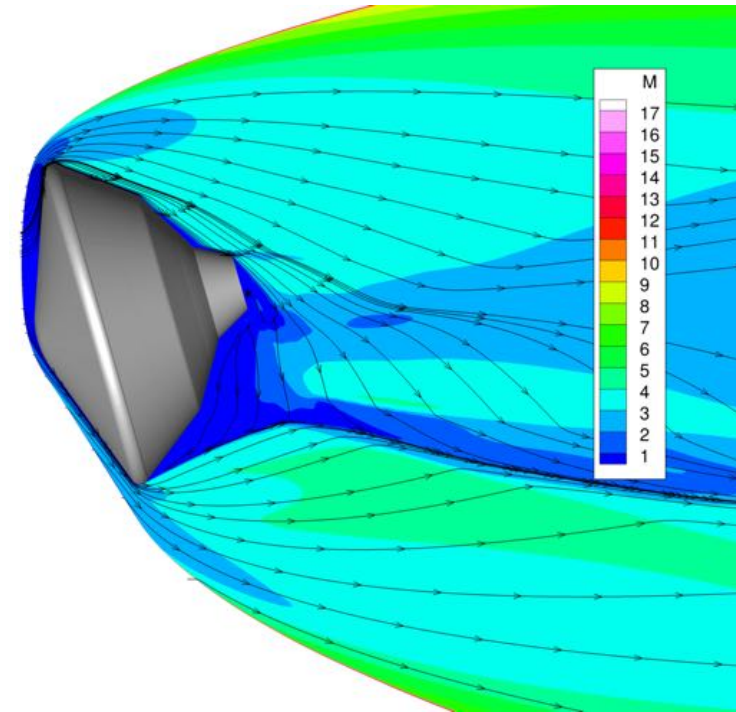




# Aerothermal environment computed from DPLR\*

## DPLR assumptions

- **Laminar** boundary layer
- **Non-blowing** & smooth wall
- Chemical and thermal non-equilibrium
- Radiative equilibrium
- Super-catalytic wall
- Mars atmosphere:  $y_{\text{CO}_2} = 0.97$ ,  $y_{\text{N}_2} = 0.03$
- 12 reactions & 8 species [12]

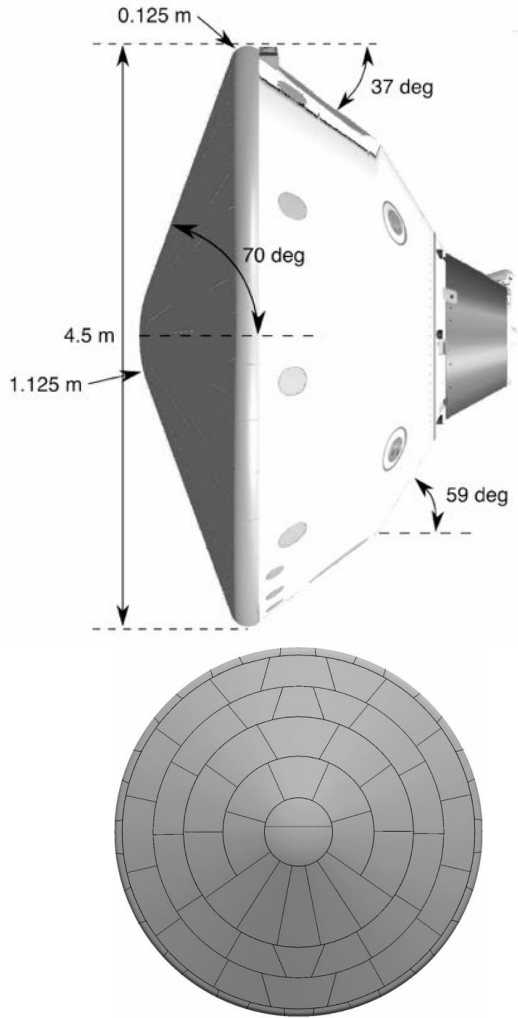


**BLAYER** calculates the **boundary layer edges** using a curvature-based method

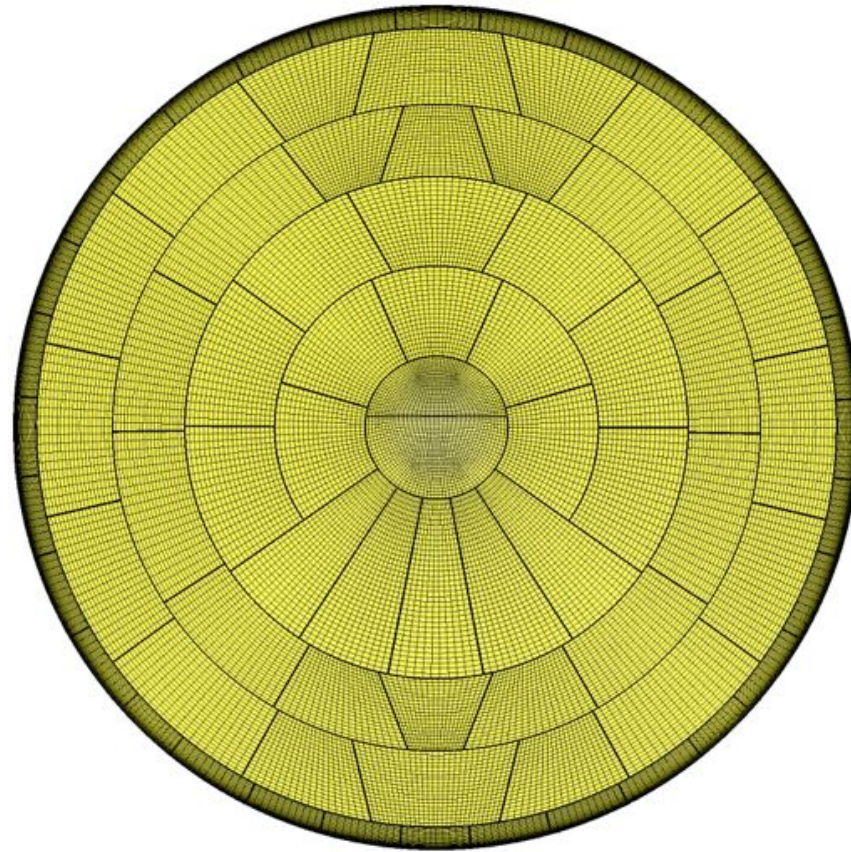
**Surface pressure  $p_w$ , heat transfer coefficient  $C_H$  and enthalpy  $h_e$  at the boundary layer edges** are used as inputs in the **material response code: PATO**

\* DPLR = Data Parallel Line Relaxation [6]

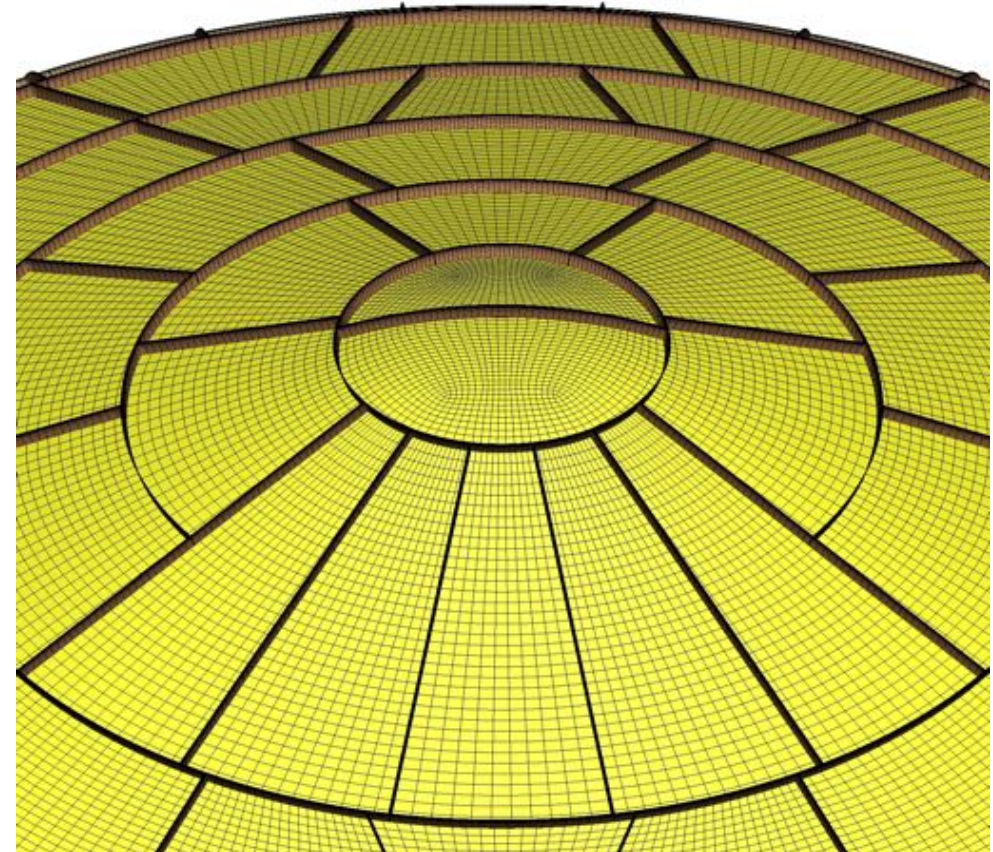
# Computational domain of the material response



**Aeroshell geometry  
with 113 PICA tiles [1]**



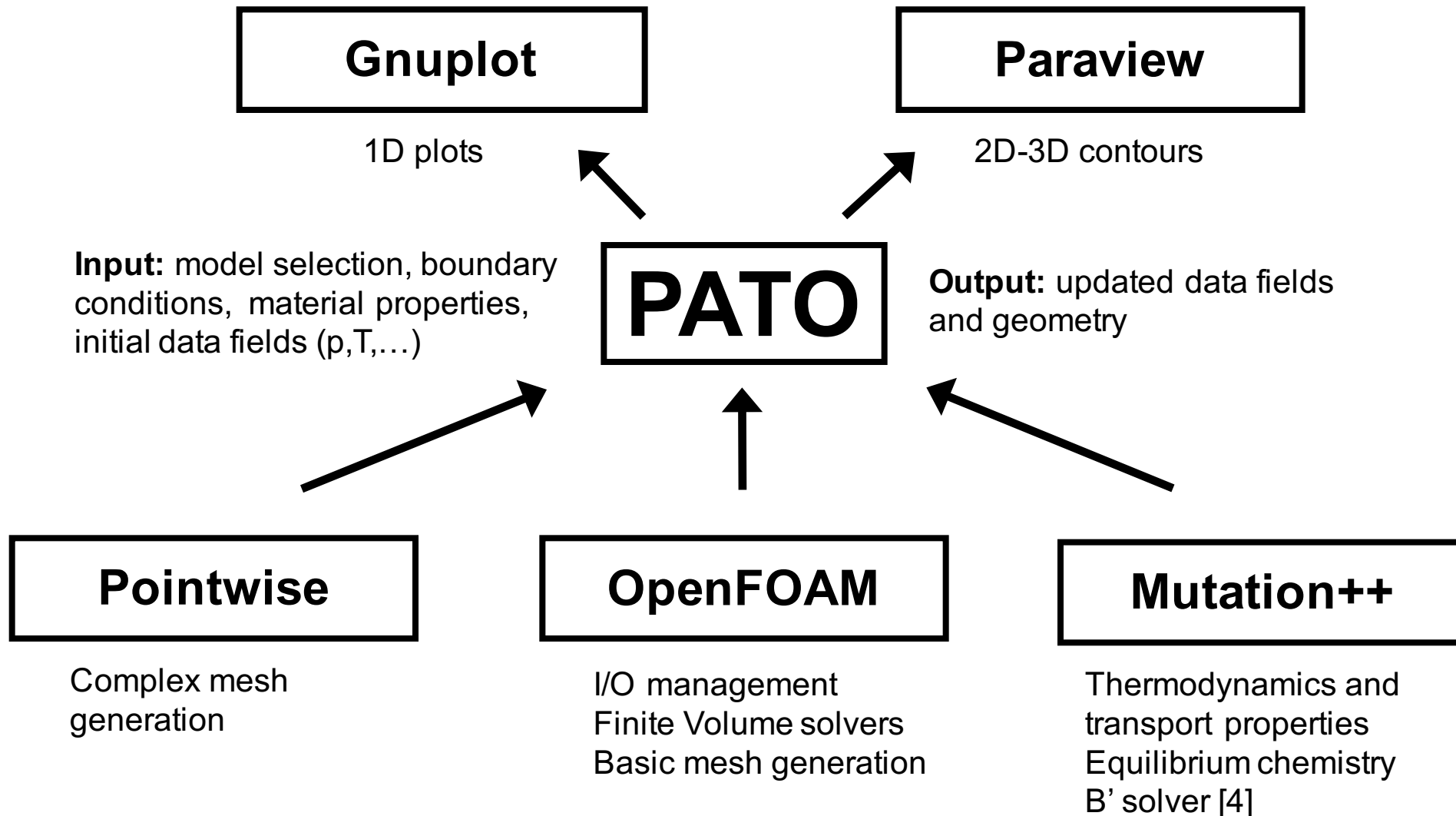
**2 million cells mesh  
of the tiled heatshield**



**Heatshield material in 2 regions  
gap filler + porous tiles**



# PATO\* is used for the material response model



\* PATO = Porous material Analysis Toolbox based on OpenFOAM [3]  
Open Source Release <http://pato.ac>

# PATO is used for the material response model

## Mass and momentum conservation

$$\mathbf{v}_g = -\frac{1}{\epsilon_g} \left( \frac{1}{\mu} \bar{\mathbf{K}} + \frac{1}{p} \bar{\mathbf{\beta}} \right) \cdot \partial_x p_g$$

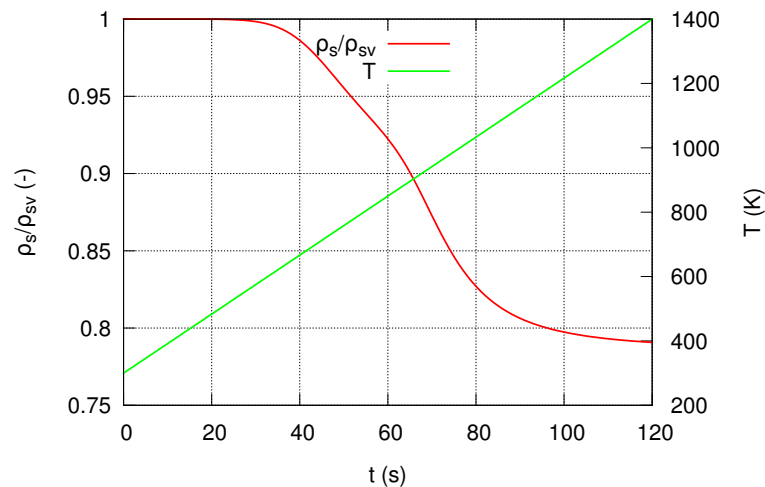
$$\partial_t \epsilon_g \rho_g - \partial_x \cdot (\epsilon_g \rho_g \mathbf{v}_g) = \Pi$$

## Pyrolysis

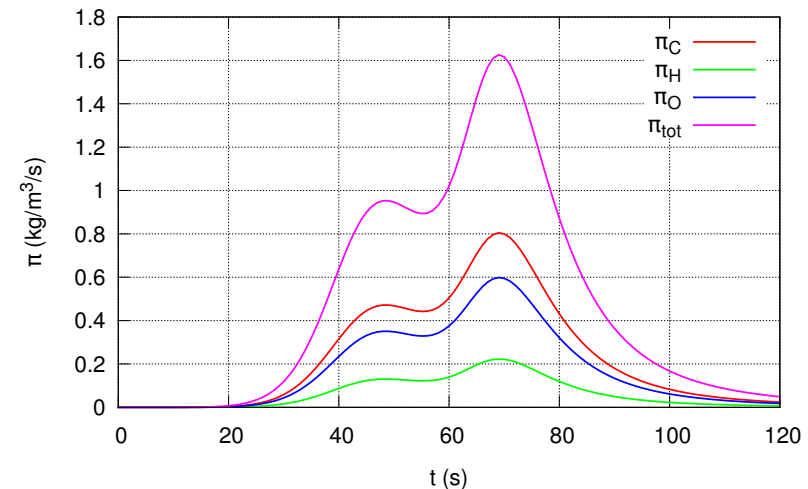
$$\partial_t \chi_{i,j} = (1 - \chi_{i,j})^{m_{i,j}} T^{n_{i,j}} A_{i,j} \exp\left(\frac{-E_{i,j}}{RT}\right)$$

$$\Pi = \sum_{i=1}^{N_p} \sum_{j=1}^{P_i} \sum_{k=1}^{N_g} \zeta_{i,j,k} \epsilon_{i,0} \rho_{i,0} F_{i,j} \partial_t \chi_{i,j}$$

Mass loss and temperature



Pyrolysis production rates



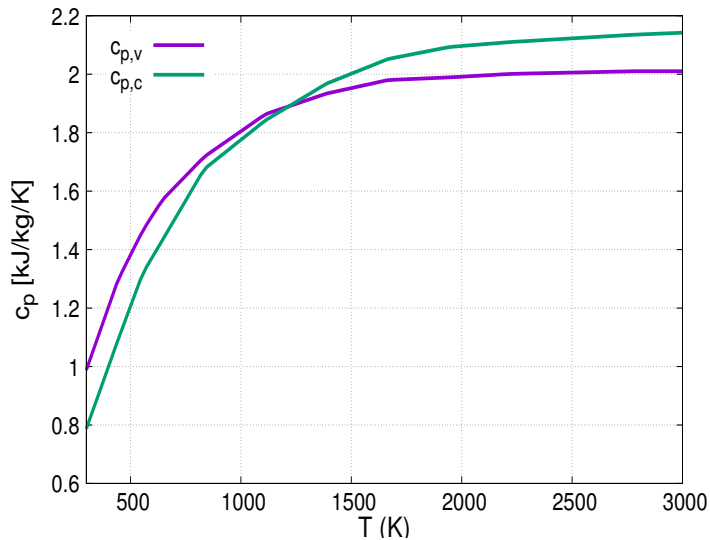
# PATO is used for the material response model

## Energy conservation

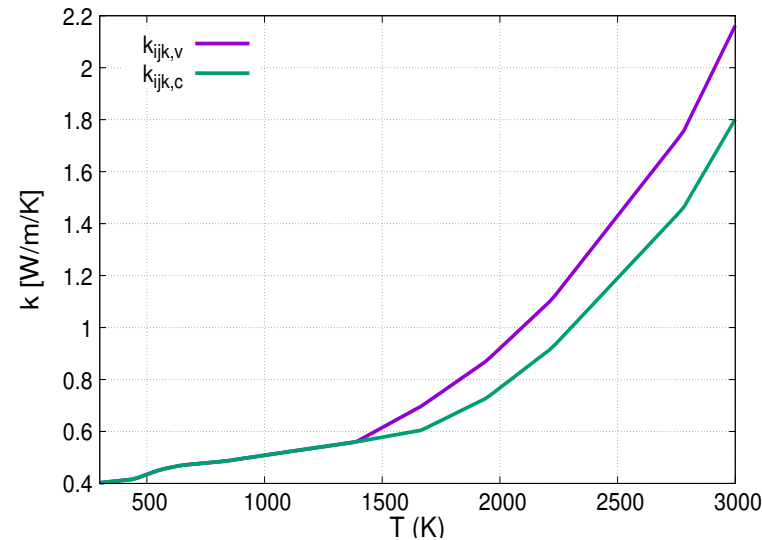
$$\sum_{i=1}^{N_p} [(\epsilon_i \rho_i c_{p,i}) \partial_t T] - \partial_x \cdot (\bar{\bar{k}} \partial_x T) = \sum_{i=1}^{N_p} [h_i \partial_t (\epsilon_i \rho_i)] - \partial_t (\epsilon_g \rho_g h_g - \epsilon_g p_g) + \partial_x \cdot (\epsilon_g \rho_g h_g \mathbf{v}_g)$$

## Isotropic TACOT properties

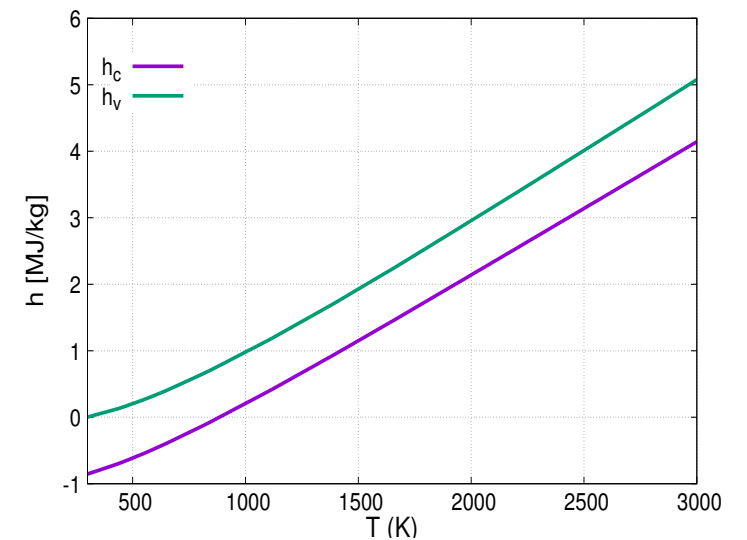
Virgin and char specific heat



Virgin and char thermal conductivity [13]



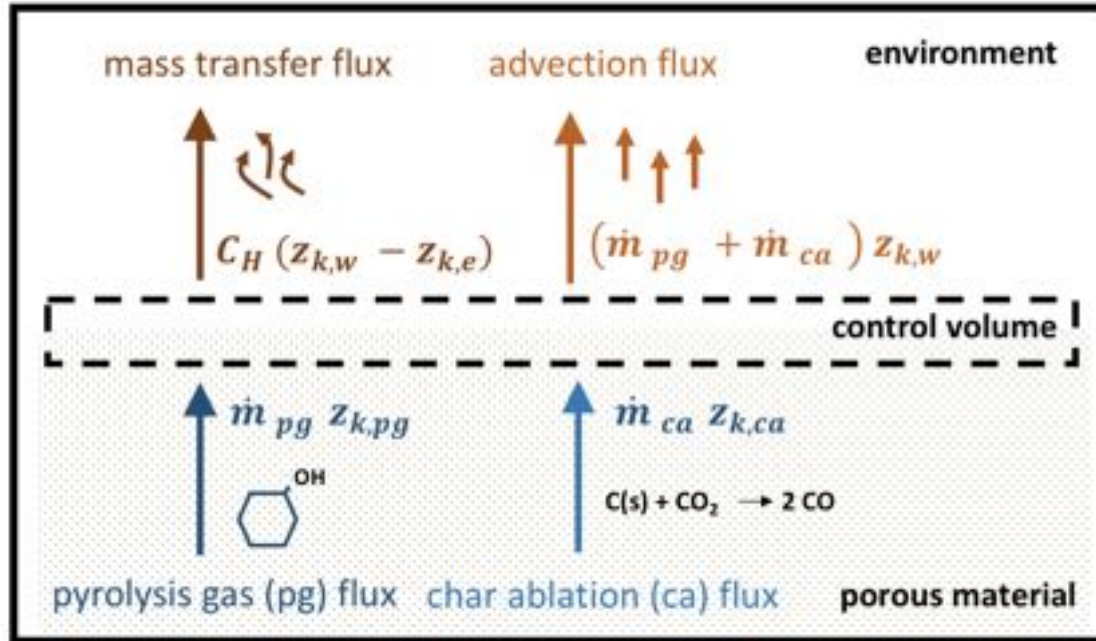
Virgin and char enthalpy



# PATO is used for the material response model

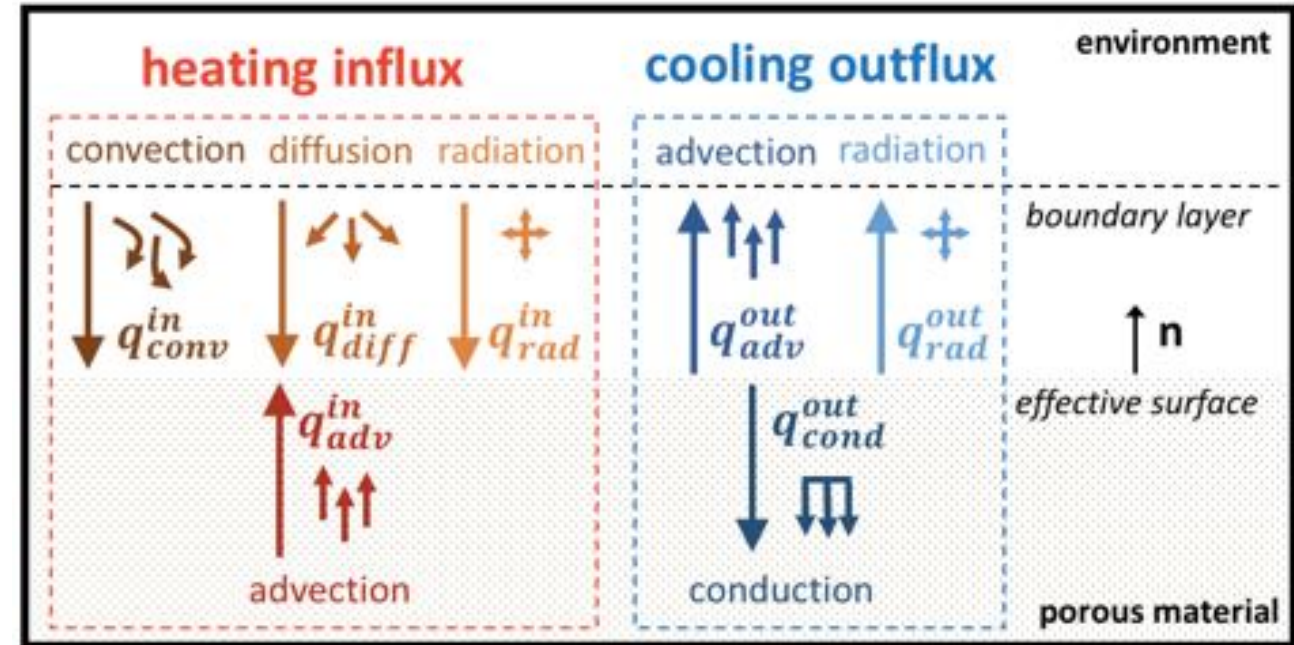
## Boundary Conditions

Surface mass balance [7]



Enthalpy at the wall  $h_w$   
 Char ablation rate  $\dot{m}_{ca}$

Surface energy balance [8,9]

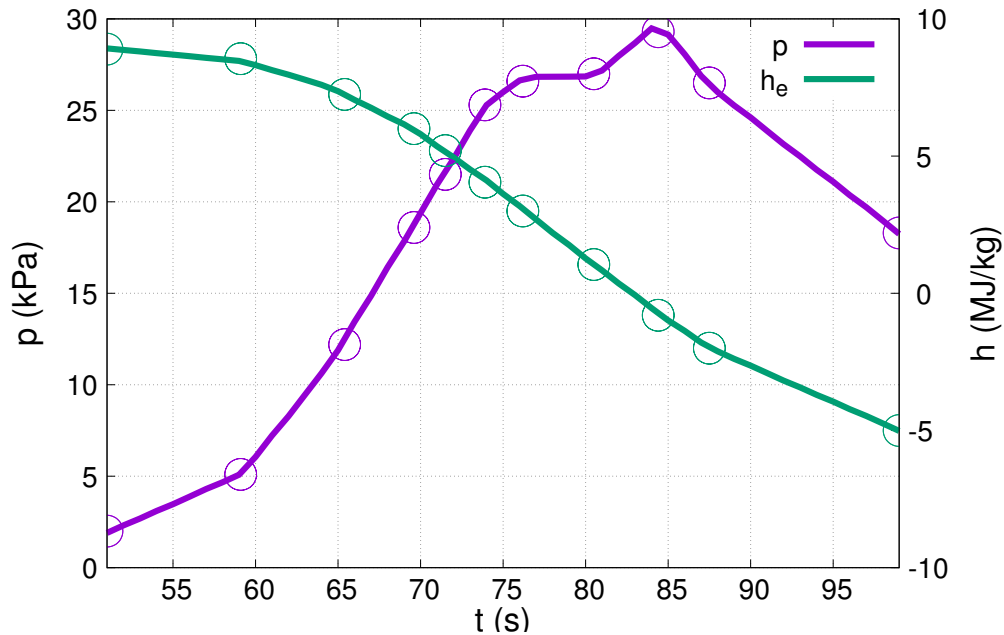


Temperature at the wall  $T_w$



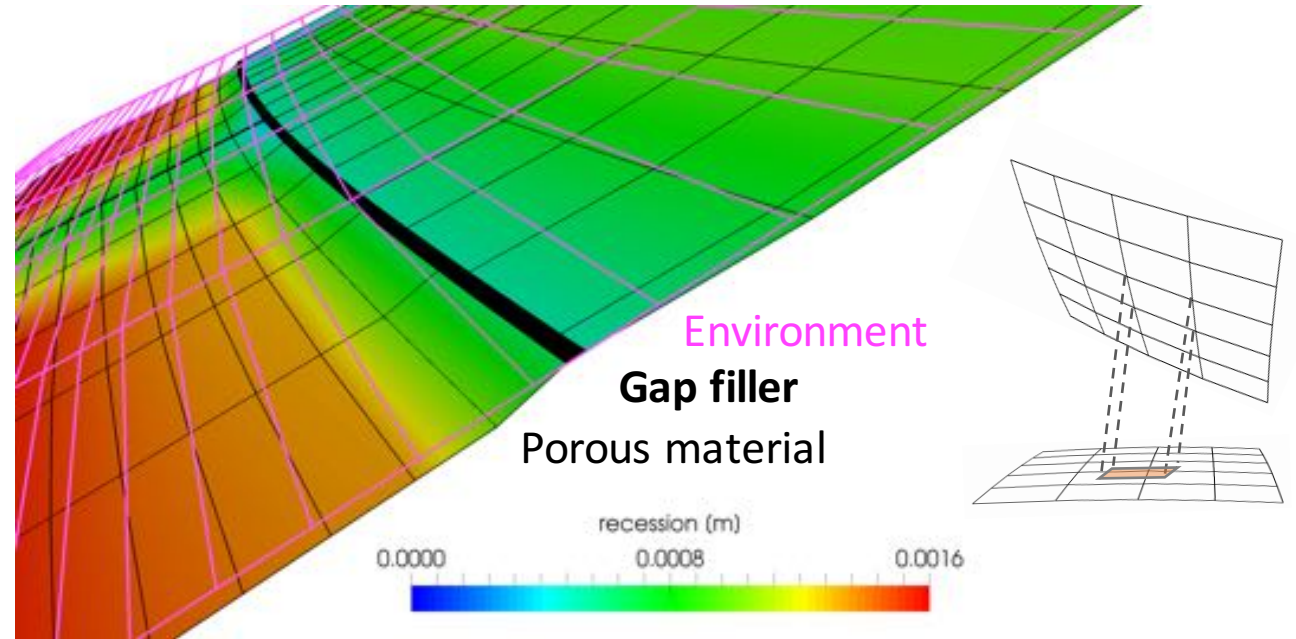
# Temporal and spatial interpolations

## Temporal interpolation



11 **discrete** times  
(50s to 100s of MSL entry)  
**linear** interpolation

## Spatial interpolation



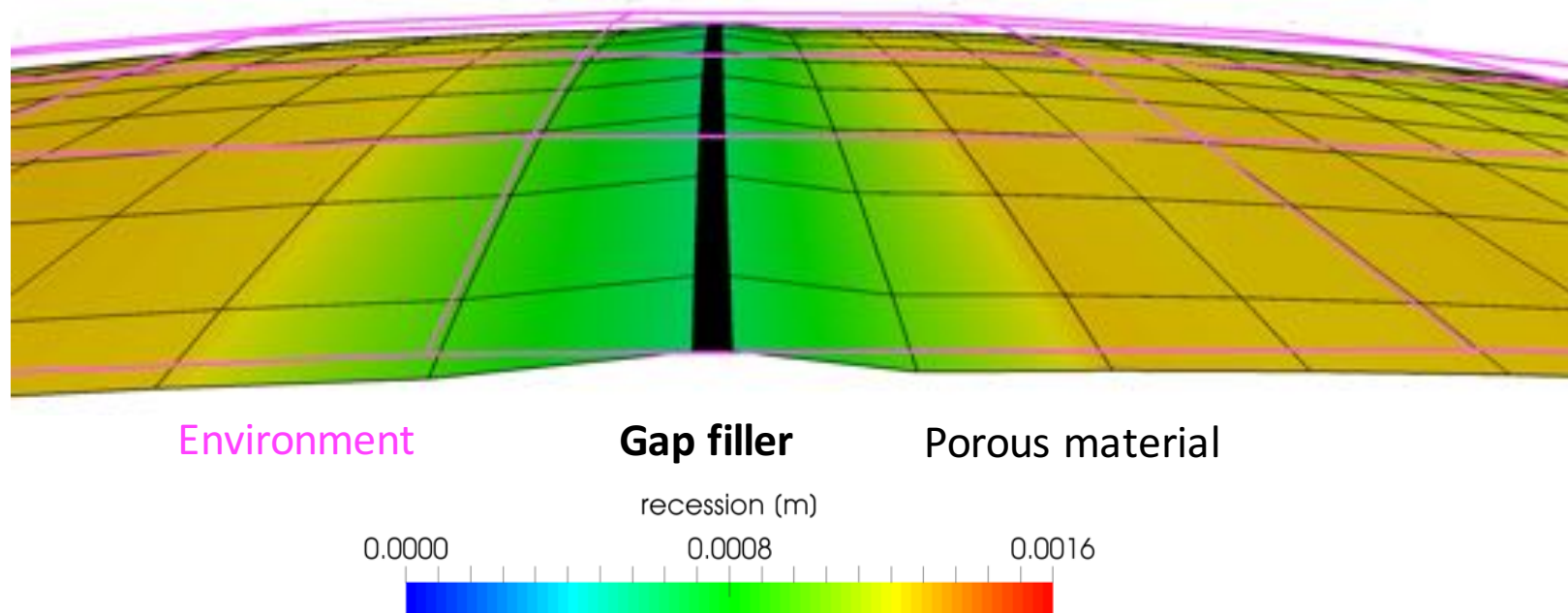
Separate mesh regions are numerically **connected** by the **Arbitrary Mesh Interface (AMI)** utility using local **Galerkin projection** [10] implemented in **OpenFOAM**

# “Fencing” effect at tile interfaces

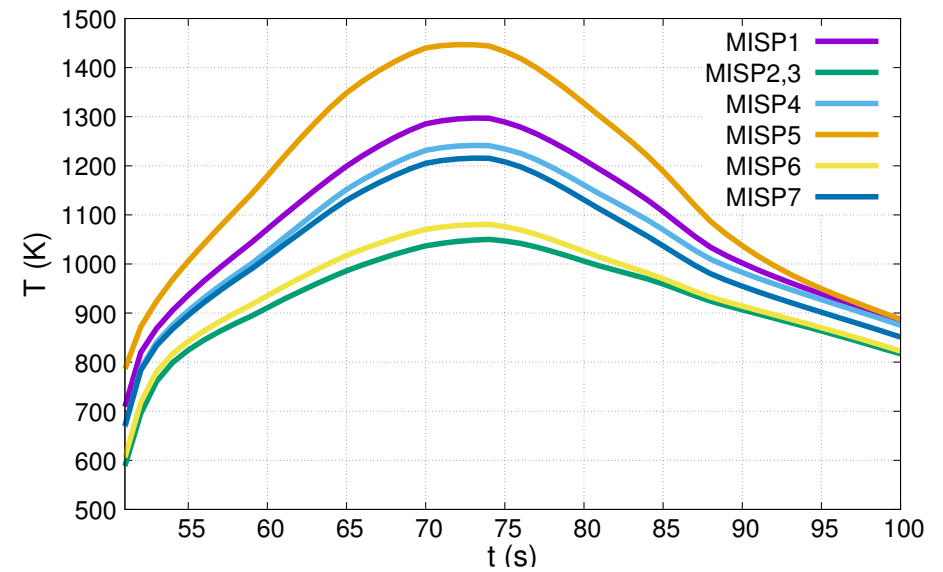
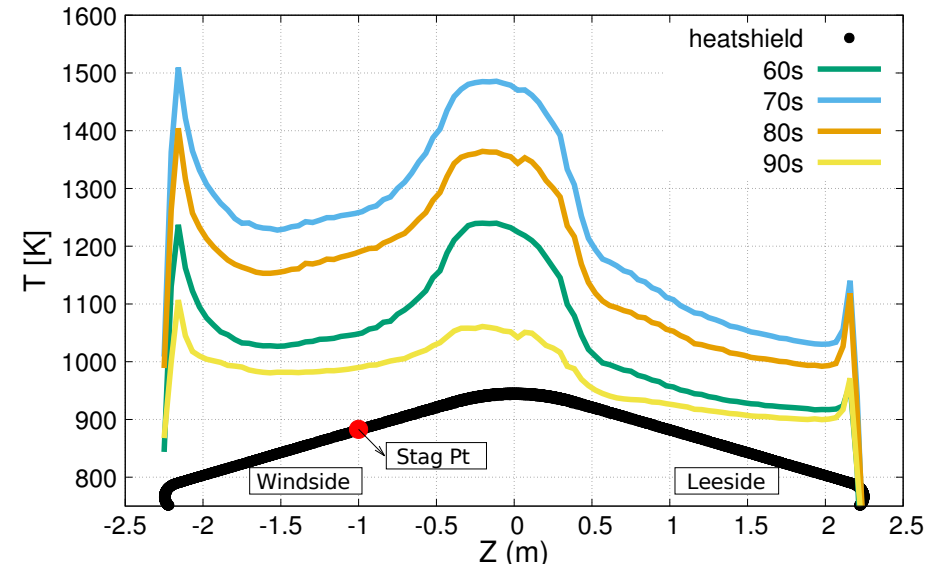
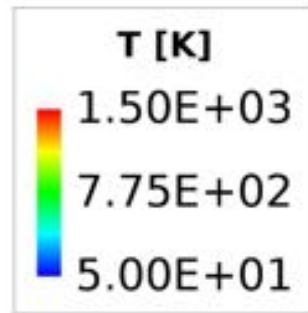
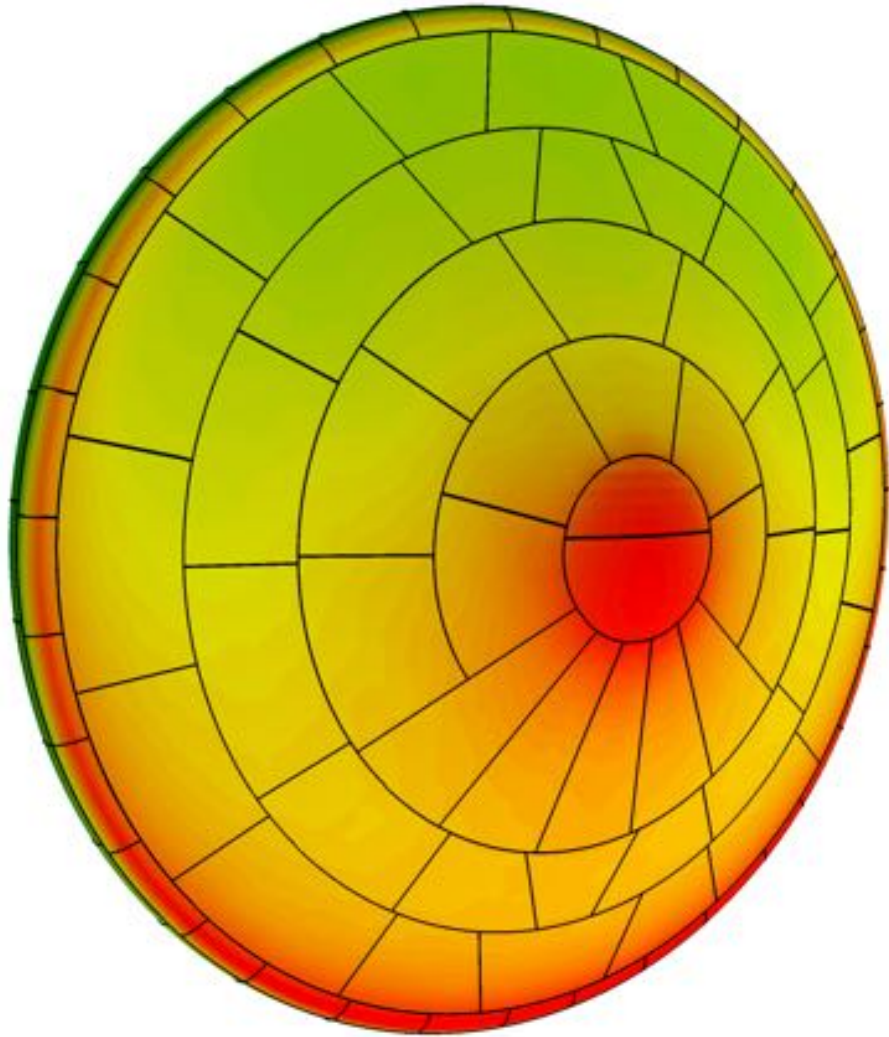
Post-test  
arcjet coupons [5]



MSL heatshield  
front surface  
at the nose

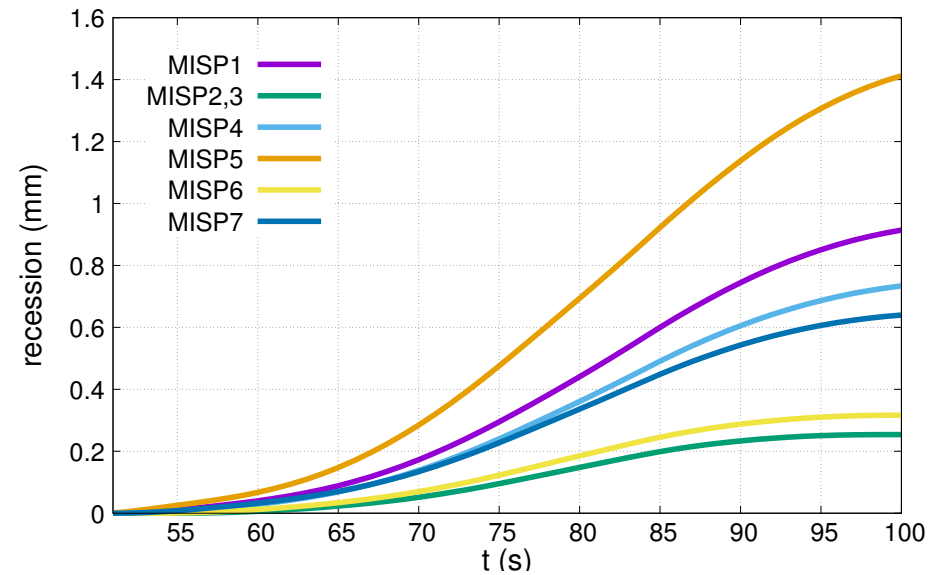
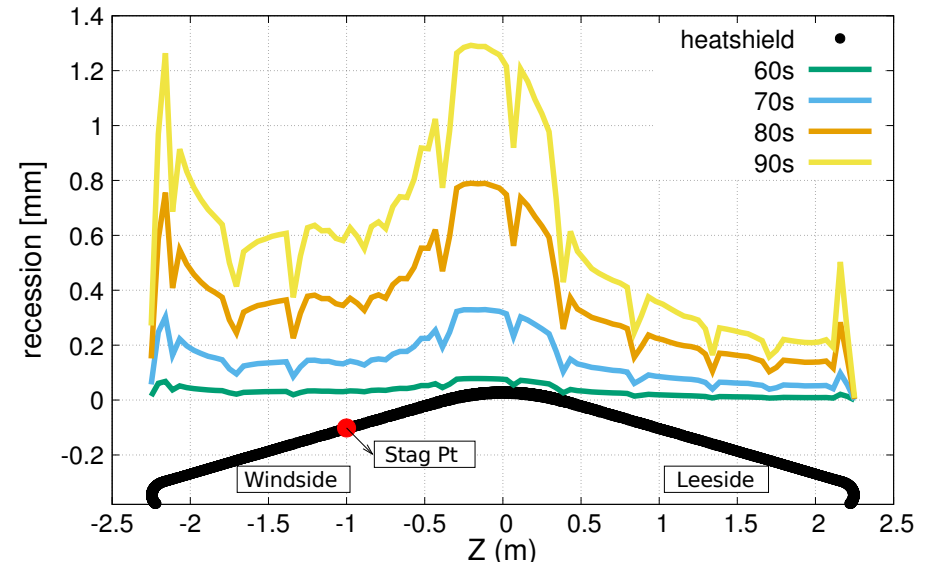
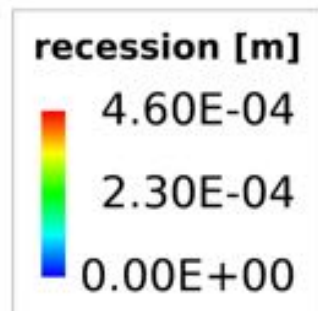
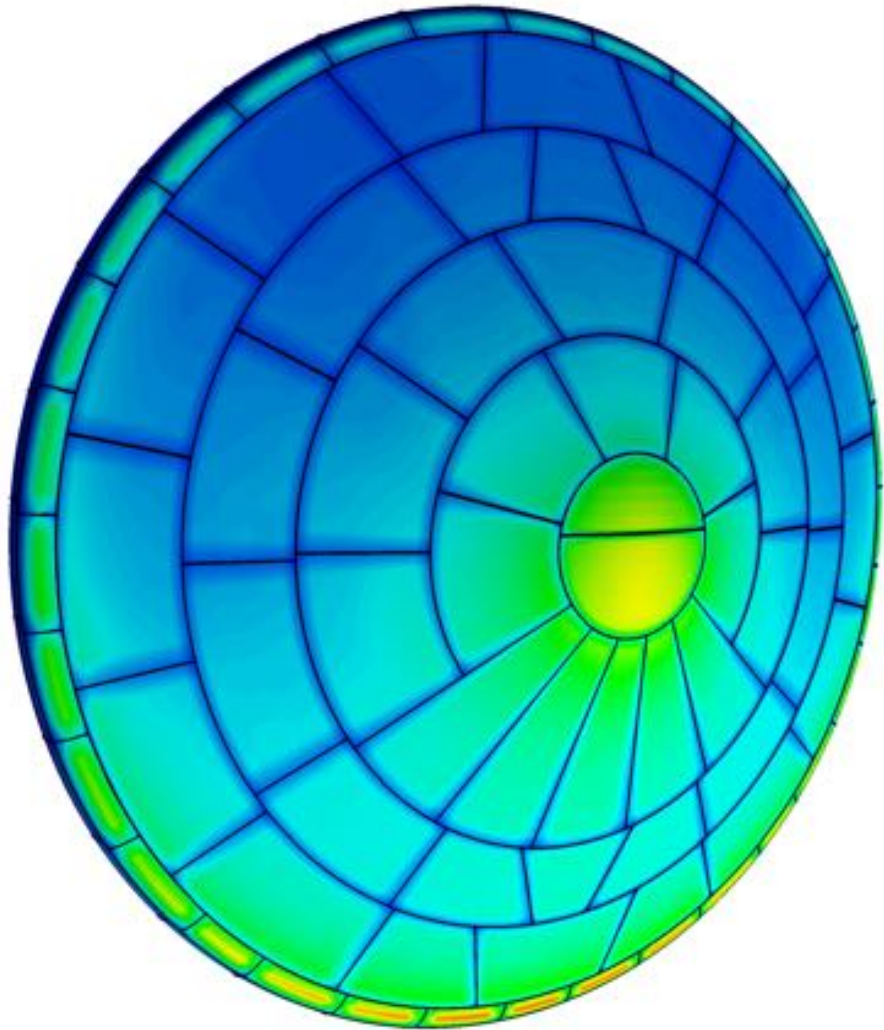


# Temperature from PATO



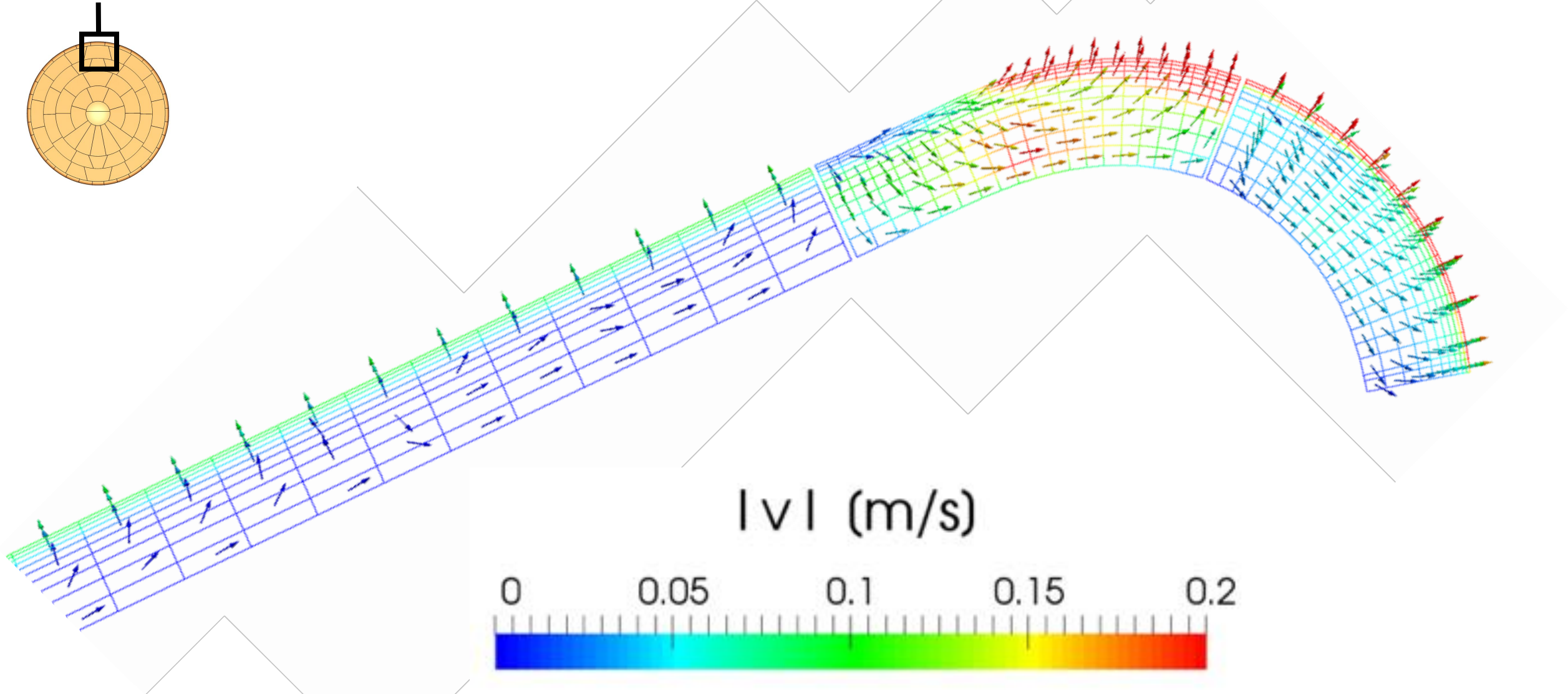
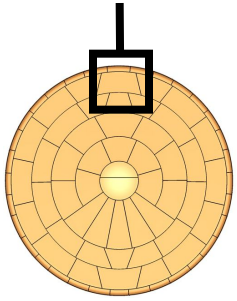


# Recession from PATO

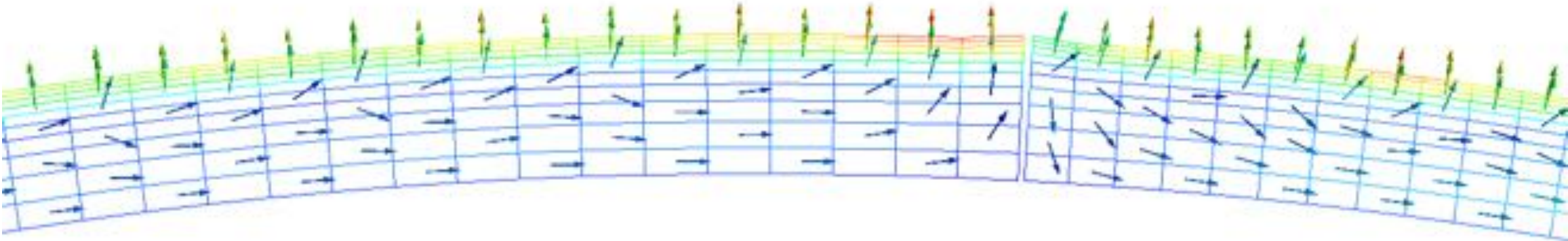
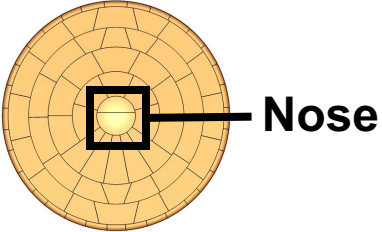


# Velocity inside the porous material

Leeside



# Velocity inside the porous material



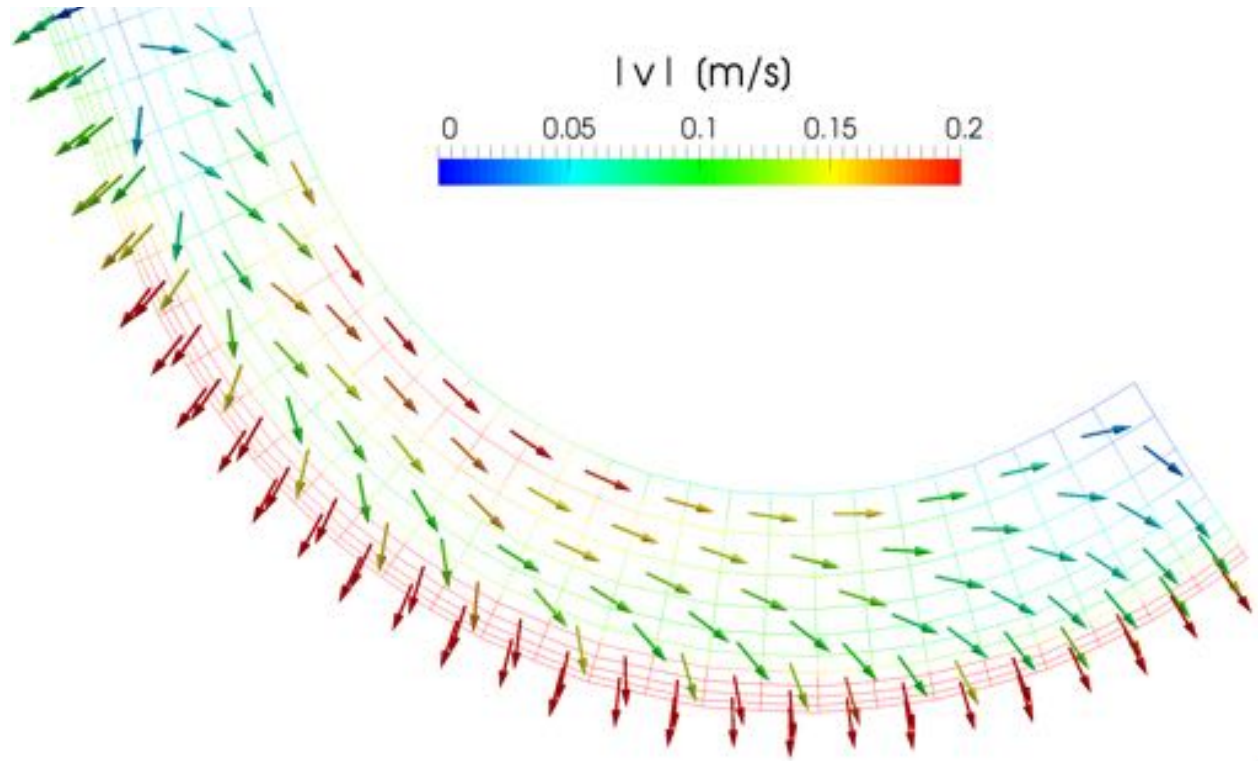
$|v|$  (m/s)



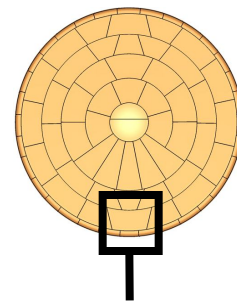
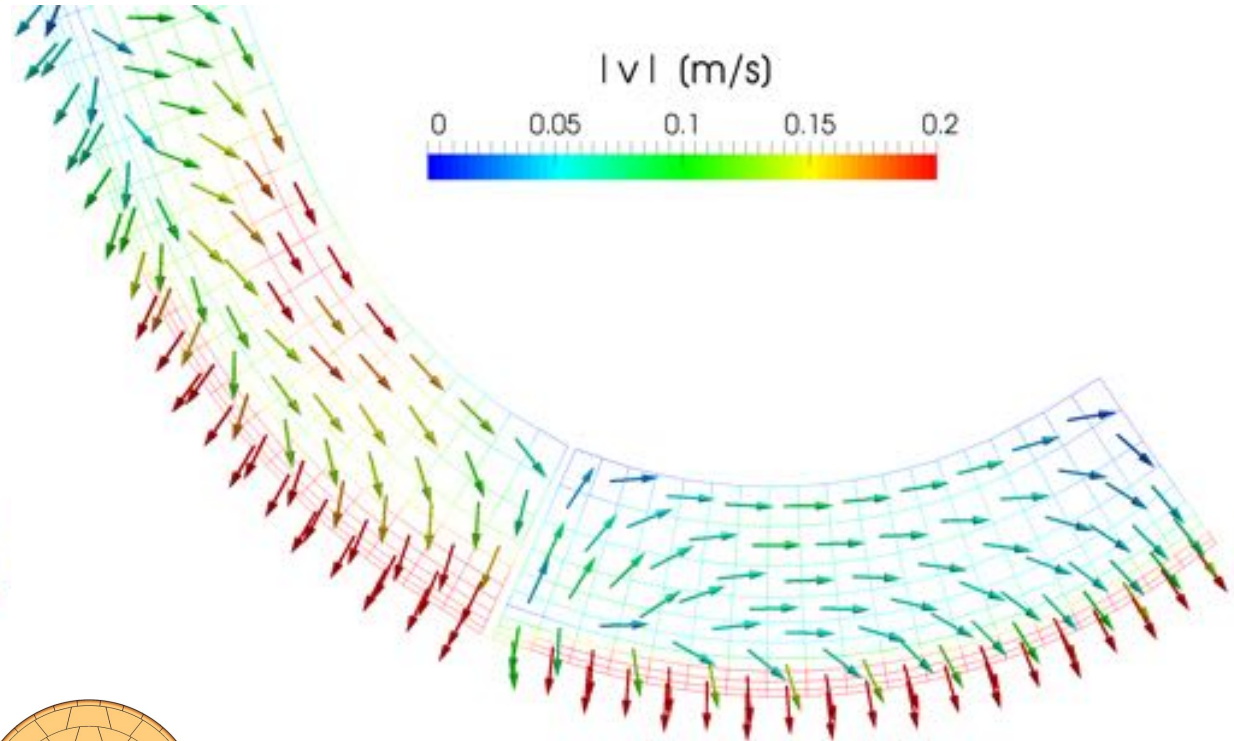


# Tiled configuration changes the flow inside the material

**Monolithic configuration**

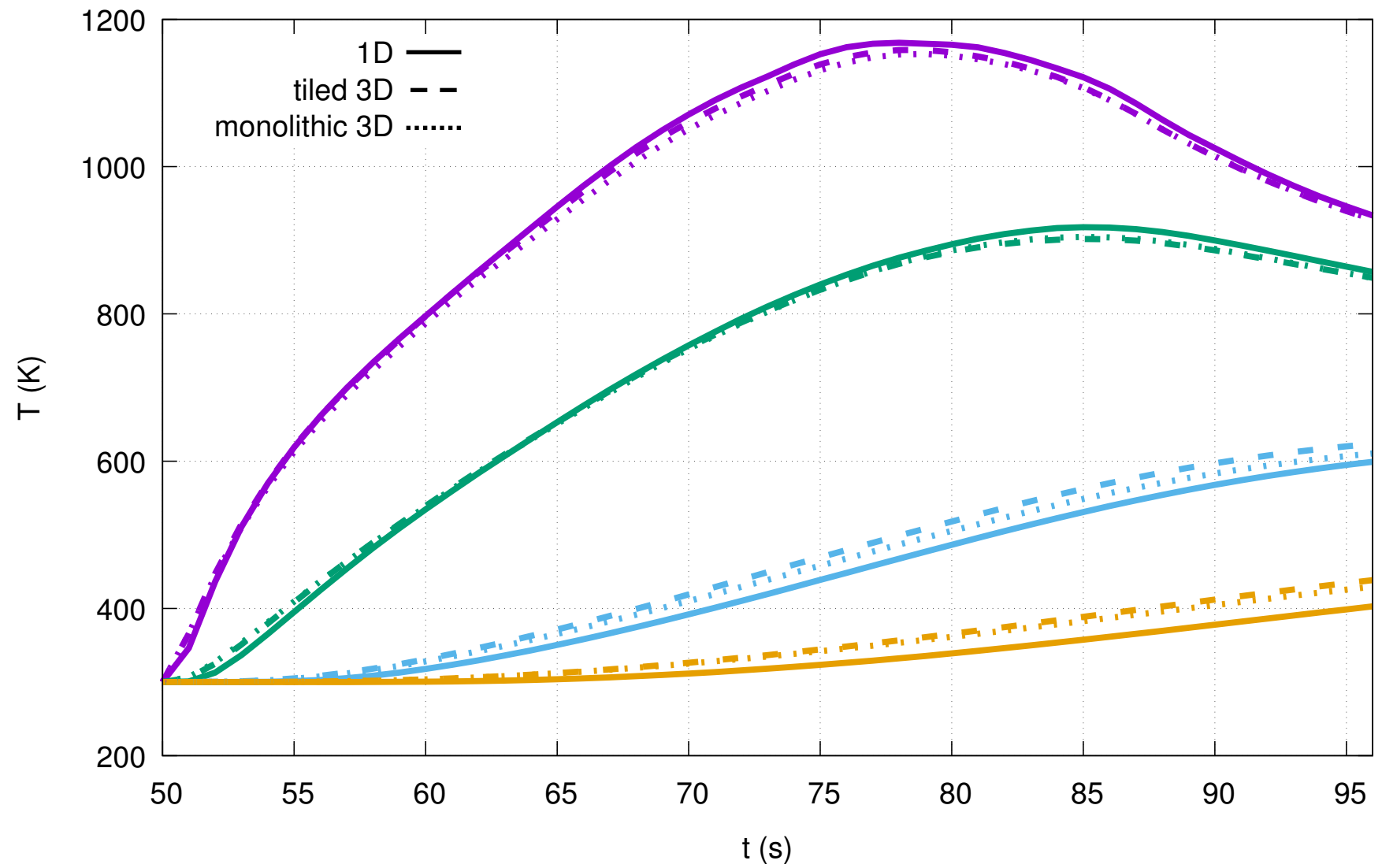
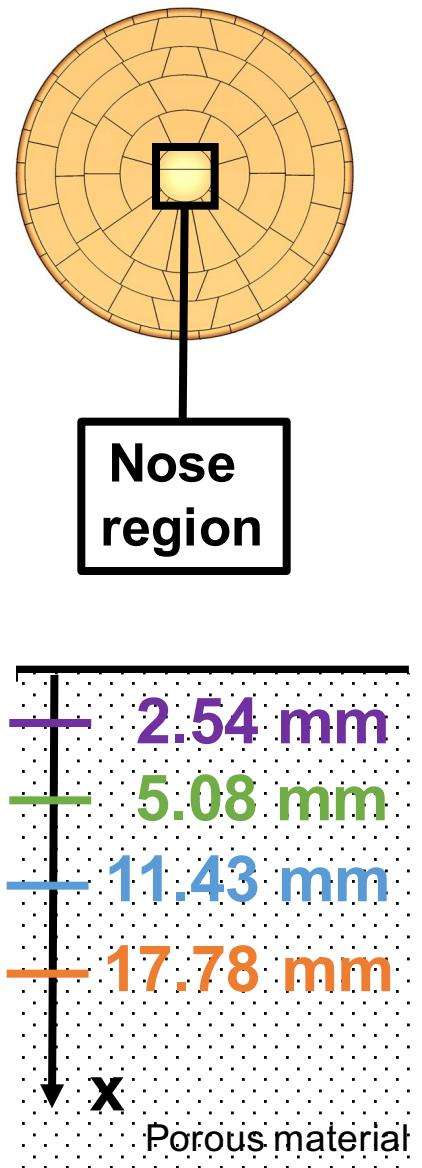


**Tiled configuration**

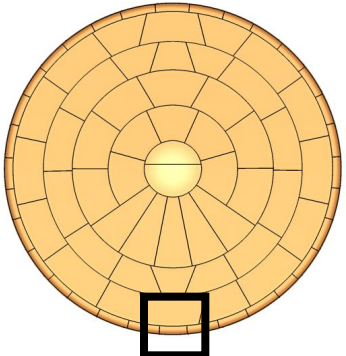


**Windside**

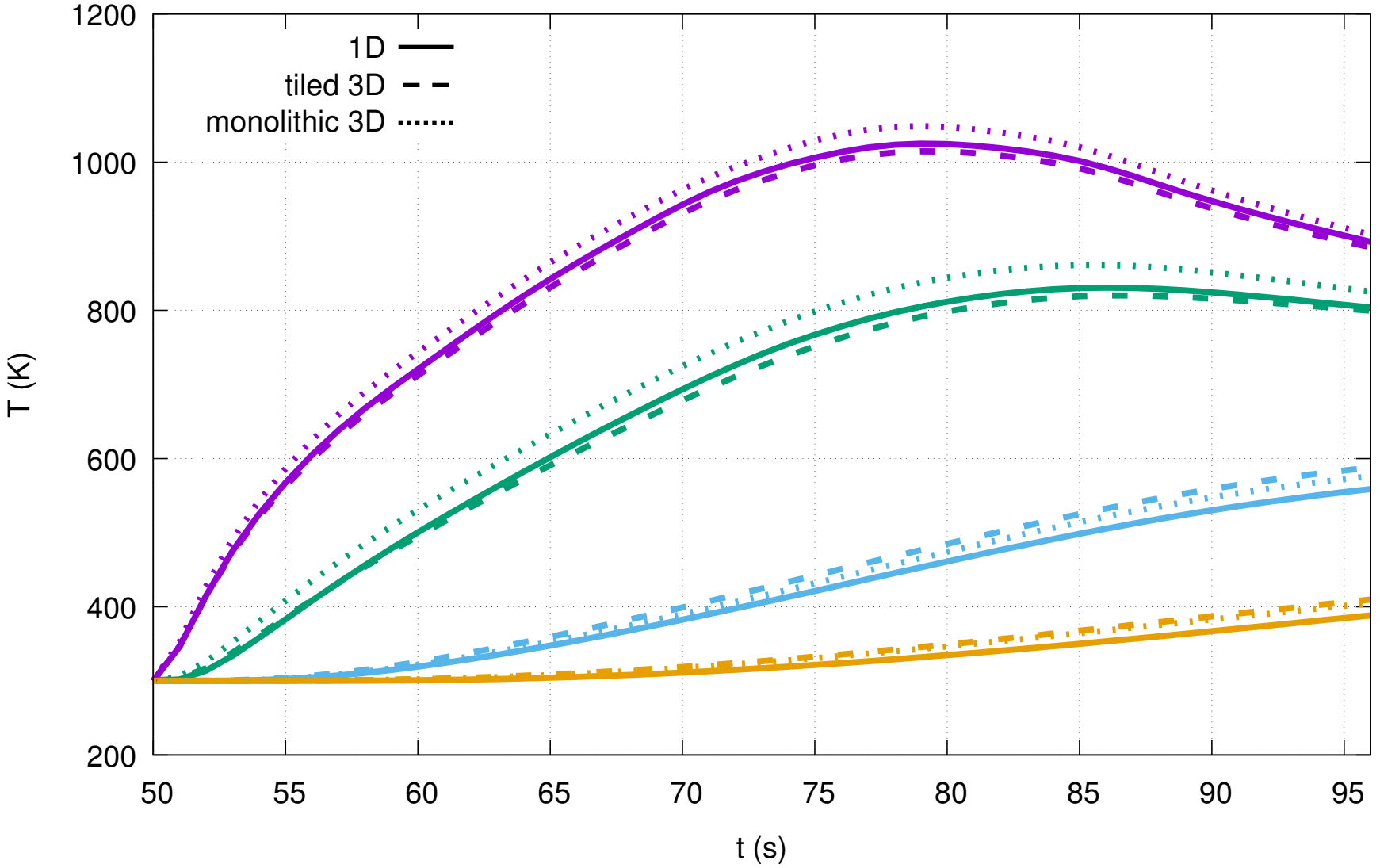
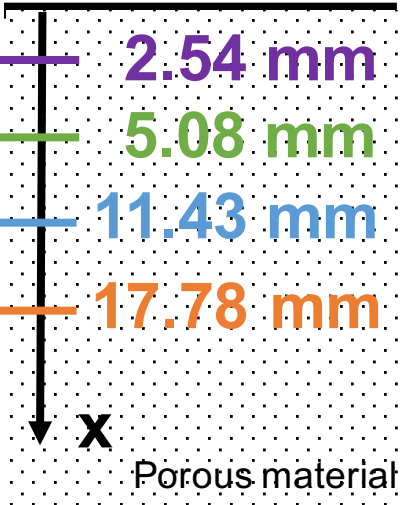
# 1D and 3D material response comparison – nose



# 1D and 3D material response comparison – shoulder



Windside  
heatshield  
shoulder





# Future work

## Hypersonic environment (DPLR)

- Laminar
- Super-catalytic wall
- Non-blowing
- 8 species & 12 reactions

↓ **New technology**

- 2020 mission
- Non-uniform thickness
- Transient turbulent
- MMOD & micro-scale

## Strong coupling



Linear in time  
Conservative in space by  
local Galerkin projection



Future work includes  
blowing from pyrolysis &  
moving mesh from recession

## New technology



PATO is capable of  
massively parallel computing  
for material response

## Porous material response (PATO)

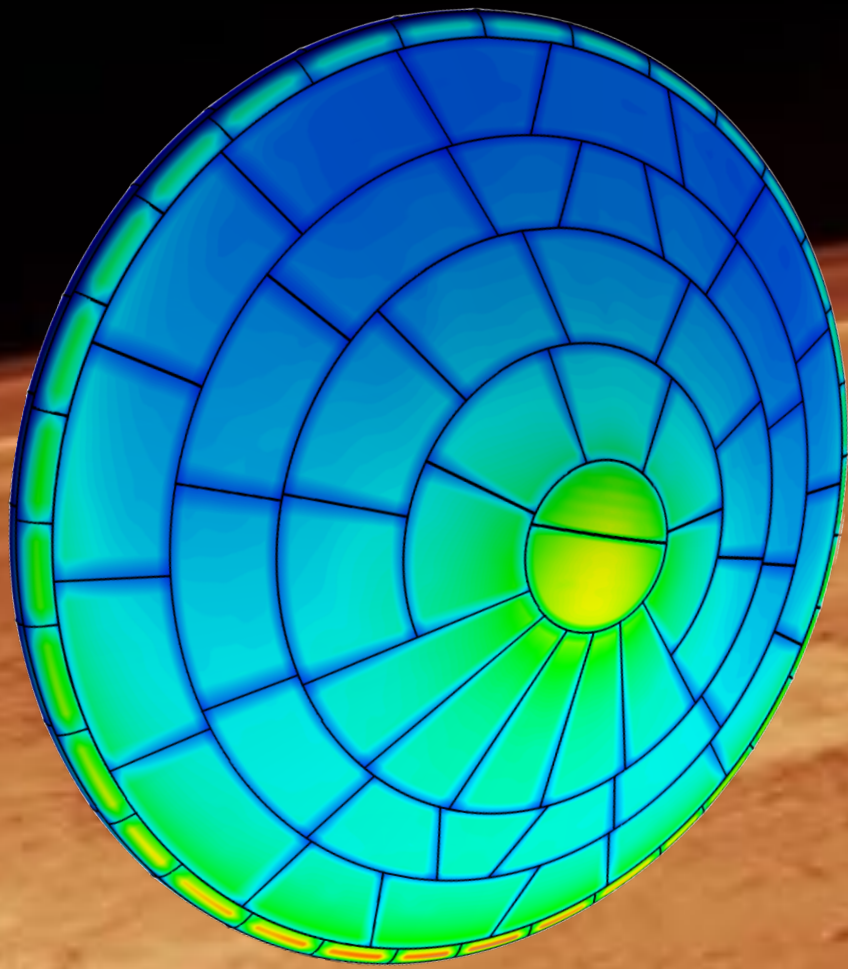
- Pyrolysis
- CMA-type BL approx.
- No finite-rate
- Equilibrium

↓ **Outputs**

- Monolithic & tiled
- Temperature 1D & 3D
- Recession 1D & 3D
- Internal velocity

# References

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- [11] A. Borner, F. Panerai, N. N. Mansour, High temperature permeability of fibrous materials using direct simulation monte carlo, *International Journal of Heat and Mass Transfer* 106 (2017) 1318 – 1326.
- [12] R. A. Mitcheltree, P. A. Gnoffo, Wake flow about a MESUR mars entry vehicle, AIAA paper 1958 (1994) 1994.
- [13] J.C. Ferguson, F. Panerai, J. Lachaud, A. Martin, S.C. Bailey, N.N. Mansour, Modeling the oxidation of low-density carbon fiber material based on microtomography, *Carbon* 96 (2016) 57–65.



# Questions ?

## 9<sup>th</sup> Ablation Workshop

Montana State University, August 30<sup>th</sup> - 31<sup>st</sup>, 2017

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